

Effects of transients in LIGO suspensions on searches for gravitational waves

LIGO Scientific Collaboration; Virgo Collaboration

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Effects of transients in LIGO suspensions on searches for gravitational waves ^F

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M. Walker ^{id}, T. D. Abbott, S. M. Aston, G. González, D. M. Macleod, J. McIver, B. P. Abbott, R. Abbott, C. Adams, R. X. Adhikari, S. B. Anderson, A. Ananyeva, S. Appert, K. Arai, S. W. Ballmer, D. Barker, B. Barr, L. Barsotti, J. Bartlett, I. Bartos, J. C. Batch, A. S. Bell ^{id}, J. Betzwieser, G. Billingsley, J. Birch, S. Biscans, C. Biwer, C. D. Blair, R. Bork, A. F. Brooks, G. Ciani, F. Clara, S. T. Countryman, M. J. Cowart, D. C. Coyne ^{id}, A. Cumming, L. Cunningham, K. Danzmann, C. F. Da Silva Costa, E. J. Daw, D. DeBra, R. T. DeRosa, R. DeSalvo, K. L. Dooley, S. Doravari, J. C. Driggers ^{id}, S. E. Dwyer, A. Effler, T. Etzel, M. Evans, T. M. Evans, M. Factourovich, H. Fair, A. Fernández Galiana ^{id}, R. P. Fisher, P. Fritschel, V. V. Frolov, P. Fulda, M. Fyffe, J. A. Giaime, K. D. Giardina, E. Goetz, R. Goetz, S. Gras, C. Gray, H. Grote, K. E. Gushwa, E. K. Gustafson, R. Gustafson, E. D. Hall, G. Hammond, J. Hanks, J. Hanson, T. Hardwick, G. M. Harry ^{id}, M. C. Heintze, A. W. Heptonstall, J. Hough, K. Izumi, R. Jones, S. Kandhasamy, S. Karki, M. Kasprzak, S. Kaufer, K. Kawabe, N. Kijbunchoo, E. J. King, P. J. King, J. S. Kissel, W. Z. Korth, G. Kuehn, M. Landry, B. Lantz, N. A. Lockerbie, M. Lormand, A. P. Lundgren, M. MacInnis, S. Márka, Z. Márka, A. S. Markosyan, E. Maros, I. W. Martin, D. V. Martynov, K. Mason, T. J. Massinger, F. Matichard, N. Mavalvala, R. McCarthy, D. E. McClelland, S. McCormick, G. McIntyre, G. Mendell, E. L. Merilh, P. M. Meyers, J. Miller, R. Mittleman, G. Moreno, G. Mueller, A. Mullavey, J. Munch, L. K. Nuttall, J. Oberling, M. Oliver, P. Oppermann, Richard J. Oram, B. O'Reilly, D. J. Ottaway, H. Overmier, J. R. Palamos, H. R. Paris, W. Parker, A. Pele, S. Penn, M. Phelps, V. Pierro, I. Pinto, M. Principe ^{id}, L. G. Prokhorov, O. Puncken, V. Quetschke, E. A. Quintero, F. J. Raab, H. Radkins, P. Raffai, S. Reid, D. H. Reitze, N. A. Robertson, J. G. Rollins, V. J. Roma, J. H. Romie, S. Rowan, K. Ryan, T. Sadecki, E. J. Sanchez, V. Sandberg, R. L. Savage, R. M. S. Schofield, D. Sellers, D. A. Shaddock, T. J. Shaffer, B. Shapiro, P. Shawhan ^{id}, D. H. Shoemaker, D. Sigg, B. J. J. Slagmolen, B. Smith, J. R. Smith, B. Sorazu ^{id}, A. Staley, K. A. Strain, D. B. Tanner, R. Taylor, M. Thomas, P. Thomas, K. A. Thorne, E. Thrane, C. I. Torrie, G. Traylor, D. Tuyenbayev, G. Vajente, G. Valdes, A. A. van Veggel, A. Vecchio, P. J. Veitch, K. Venkateswara, T. Vo, C. Vorvick, R. L. Ward, J. Warner, B. Weaver, R. Weiss, P. Weßels, B. Willke, C. C. Wipf, J. Worden, G. Wu, H. Yamamoto, C. C. Yancey, Hang Yu, Haocun Yu, L. Zhang, M. E. Zucker, and J. Zweizig

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Effects of transients in LIGO suspensions on searches for gravitational waves

M. Walker,^{1,2} T. D. Abbott,¹ S. M. Aston,³ G. González,¹ D. M. Macleod,¹ J. McIver,⁴ B. P. Abbott,⁴ R. Abbott,⁴ C. Adams,³ R. X. Adhikari,⁴ S. B. Anderson,⁴ A. Ananyeva,⁴ S. Appert,⁴ K. Arai,⁴ S. W. Ballmer,⁵ D. Barker,⁶ B. Barr,⁷ L. Barsotti,⁸ J. Bartlett,⁶ I. Bartos,⁹ J. C. Batch,⁶ A. S. Bell,⁷ J. Betzwieser,³ G. Billingsley,⁴ J. Birch,³ S. Biscans,^{4,8} C. Biwer,⁵ C. D. Blair,¹⁰ R. Bork,⁴ A. F. Brooks,⁴ G. Ciani,¹¹ F. Clara,⁶ S. T. Countryman,⁹ M. J. Cowart,³ D. C. Coyne,⁴ A. Cumming,⁷ L. Cunningham,⁷ K. Danzmann,^{12,13} C. F. Da Silva Costa,¹¹ E. J. Daw,¹⁴ D. DeBra,¹⁵ R. T. DeRosa,³ R. DeSalvo,¹⁶ K. L. Dooley,¹⁷ S. Doravari,³ J. C. Driggers,⁶ S. E. Dwyer,⁶ A. Effler,³ T. Etzel,⁴ M. Evans,⁸ T. M. Evans,³ M. Factourovich,⁹ H. Fair,⁵ A. Fernández Galiana,⁸ R. P. Fisher,⁵ P. Fritschel,⁸ V. V. Frolov,³ P. Fulda,¹¹ M. Fyffe,³ J. A. Giaime,^{1,3} K. D. Giardina,³ E. Goetz,¹³ R. Goetz,¹¹ S. Gras,⁸ C. Gray,⁶ H. Grote,¹³ K. E. Gushwa,⁴ E. K. Gustafson,⁴ R. Gustafson,¹⁸ E. D. Hall,⁴ G. Hammond,⁷ J. Hanks,⁶ J. Hanson,³ T. Hardwick,¹ G. M. Harry,¹⁹ M. C. Heintze,³ A. W. Heptonstall,⁴ J. Hough,⁷ K. Izumi,⁶ R. Jones,⁷ S. Kandhasamy,¹⁷ S. Karki,²⁰ M. Kasprzak,¹ S. Kaufer,¹² K. Kawabe,⁶ N. Kijbunchoo,⁶ E. J. King,²¹ P. J. King,⁶ J. S. Kissel,⁶ W. Z. Korth,⁴ G. Kuehn,¹³ M. Landry,⁶ B. Lantz,¹⁵ N. A. Lockerbie,²² M. Lormand,³ A. P. Lundgren,¹³ M. MacInnis,⁸ S. Márka,⁹ Z. Márka,⁹ A. S. Markosyan,¹⁵ E. Maros,⁴ I. W. Martin,⁷ D. V. Martynov,⁸ K. Mason,⁸ T. J. Massinger,⁵ F. Matichard,^{4,8} N. Mavalvala,⁸ R. McCarthy,⁶ D. E. McClelland,²³ S. McCormick,³ G. McIntyre,⁴ G. Mendell,⁶ E. L. Merilh,⁶ P. M. Meyers,²⁴ J. Miller,⁸ R. Mittleman,⁸ G. Moreno,⁶ G. Mueller,¹¹ A. Mullavey,³ J. Munch,²¹ L. K. Nuttall,⁵ J. Oberling,⁶ M. Oliver,²⁵ P. Oppermann,¹³ Richard J. Oram,³ B. O'Reilly,³ D. J. Ottaway,²¹ H. Overmier,³ J. R. Palamos,²⁰ H. R. Paris,¹⁵ W. Parker,³ A. Pele,³ S. Penn,²⁶ M. Phelps,⁷ V. Pierro,¹⁶ I. Pinto,¹⁶ M. Principe,¹⁶ L. G. Prokhorov,²⁷ O. Puncken,¹³ V. Quetschke,²⁸ E. A. Quintero,⁴ F. J. Raab,⁶ H. Radkins,⁶ P. Raffai,²⁹ S. Reid,³⁰ D. H. Reitze,^{4,11} N. A. Robertson,^{4,7} J. G. Rollins,⁴ V. J. Roma,²⁰ J. H. Romie,³ S. Rowan,⁷ K. Ryan,⁶ T. Sadecki,⁶ E. J. Sanchez,⁴ V. Sandberg,⁶ R. L. Savage,⁶ R. M. S. Schofield,²⁰ D. Sellers,³ D. A. Shaddock,²³ T. J. Shaffer,⁶ B. Shapiro,¹⁵ P. Shawhan,³¹ D. H. Shoemaker,⁸ D. Sigg,⁶ B. J. J. Slagmolen,²³ B. Smith,³ J. R. Smith,² B. Sorazu,⁷ A. Staley,⁹ K. A. Strain,⁷ D. B. Tanner,¹¹ R. Taylor,⁴ M. Thomas,³ P. Thomas,⁶ K. A. Thorne,³ E. Thrane,³² C. I. Torrie,⁴ G. Traylor,³ D. Tuyenbayev,²⁸ G. Vajente,⁴ G. Valdes,²⁸ A. A. van Veggel,⁷ A. Vecchio,³³ P. J. Veitch,²¹ K. Venkateswara,³⁴ T. Vo,⁵ C. Vorvick,⁶ R. L. Ward,²³ J. Warner,⁶ B. Weaver,⁶ R. Weiss,⁸ P. Weßels,¹³ B. Willke,^{12,13} C. C. Wipf,⁴ J. Worden,⁶ G. Wu,³ H. Yamamoto,⁴ C. C. Yancey,³¹ Hang Yu,⁸ Haocun Yu,⁸ L. Zhang,⁴ M. E. Zucker,^{4,8} and J. Zweizig⁴

¹Louisiana State University, Baton Rouge, Louisiana 70803, USA

²California State University Fullerton, Fullerton, California 92831, USA

³LIGO Livingston Observatory, Livingston, Louisiana 70754, USA

⁴LIGO, California Institute of Technology, Pasadena, California 91125, USA

⁵Syracuse University, Syracuse, New York 13244, USA

⁶LIGO Hanford Observatory, Richland, Washington 99352, USA

⁷SUPA, University of Glasgow, Glasgow G12 8QQ, United Kingdom

⁸LIGO, Massachusetts Institute of Technology, Cambridge, Massachusetts 02139, USA

⁹Columbia University, New York, New York 10027, USA

¹⁰University of Western Australia, Crawley, Western Australia 6009, Australia

¹¹University of Florida, Gainesville, Florida 32611, USA

¹²Leibniz Universität Hannover, D-30167 Hannover, Germany

¹³Albert-Einstein-Institut, Max-Planck-Institut für Gravitationsphysik, D-30167 Hannover, Germany

¹⁴The University of Sheffield, Sheffield S10 2TN, United Kingdom

¹⁵Stanford University, Stanford, California 94305, USA

¹⁶University of Sannio at Benevento, I-82100 Benevento, Italy and INFN, Sezione di Napoli, I-80100 Napoli, Italy

¹⁷The University of Mississippi, University, Mississippi 38677, USA

¹⁸University of Michigan, Ann Arbor, Michigan 48109, USA

¹⁹American University, Washington, D.C. 20016, USA

²⁰University of Oregon, Eugene, Oregon 97403, USA

²¹University of Adelaide, Adelaide, South Australia 5005, Australia

²²SUPA, University of Strathclyde, Glasgow G1 1XQ, United Kingdom

²³Australian National University, Canberra, Australian Capital Territory 0200, Australia

²⁴University of Minnesota, Minneapolis, Minnesota 55455, USA

²⁵Universitat de les Illes Balears, IAC3—IEEC, E-07122 Palma de Mallorca, Spain

²⁶Hobart and William Smith Colleges, Geneva, New York 14456, USA

²⁷Faculty of Physics, Lomonosov Moscow State University, Moscow 119991, Russia

²⁸The University of Texas Rio Grande Valley, Brownsville, Texas 78520, USA

²⁹MTA Eötvös University, “Lendület” Astrophysics Research Group, Budapest 1117, Hungary

³⁰SUPA, University of the West of Scotland, Paisley PA1 2BE, United Kingdom

³¹University of Maryland, College Park, Maryland 20742, USA

³²Monash University, Victoria 3800, Australia

³³University of Birmingham, Birmingham B15 2TT, United Kingdom

³⁴University of Washington, Seattle, Washington 98195, USA

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This paper presents an analysis of the transient behavior of the Advanced LIGO (Laser Interferometer Gravitational-wave Observatory) suspensions used to seismically isolate the optics. We have characterized the transients in the longitudinal motion of the quadruple suspensions during Advanced LIGO’s first observing run. Propagation of transients between stages is consistent with modeled transfer functions, such that transient motion originating at the top of the suspension chain is significantly reduced in amplitude at the test mass. We find that there are transients seen by the longitudinal motion monitors of quadruple suspensions, but they are not significantly correlated with transient motion above the noise floor in the gravitational wave strain data, and therefore do not present a dominant source of background noise in the searches for transient gravitational wave signals. Using the suspension transfer functions, we compared the transients in a week of gravitational wave strain data with transients from a quadruple suspension. Of the strain transients between 10 and 60 Hz, 84% are loud enough that they would have appeared above the sensor noise in the top stage quadruple suspension monitors if they had originated at that stage at the same frequencies. We find no significant temporal correlation with the suspension transients in that stage, so we can rule out suspension motion originating at the top stage as the cause of those transients. However, only 3.2% of the gravitational wave strain transients are loud enough that they would have been seen by the second stage suspension sensors, and none of them are above the sensor noise levels of the penultimate stage. Therefore, we cannot eliminate the possibility of transient noise in the detectors originating in the intermediate stages of the suspension below the sensing noise. *Published by AIP Publishing.* <https://doi.org/10.1063/1.5000264>

I. INTRODUCTION

The Laser Interferometer Gravitational-wave Observatory (LIGO) was designed to detect gravitational waves from astrophysical sources.^{1,2} After six science runs over the course of several years, the detectors underwent major upgrades starting in 2010. In September 2015, the newly upgraded Advanced LIGO detectors began taking data for their first observational period (O1). Figure 1 shows the basic optical configuration of Advanced LIGO. With a sensitivity more than three times better than that of the previous generation,³ the detectors had the astrophysical reach to make the first direct observation of a gravitational wave signal, GW150914, from the merger of two black holes,⁴ and later a second unambiguous detection, GW151226.⁵ These observations have opened a new field of gravitational-wave astronomy, which will continue to grow brighter with further improvements to the detector network.

The main limitation to LIGO’s low-frequency (up to 10 Hz) sensitivity is seismic noise. (At intermediate frequencies, technical noises and thermal noise of the mirror coatings are the dominant source of noise, and at frequencies higher than 100 Hz, the detectors are limited by photon shot noise.)² The LIGO detectors are affected by earthquakes from around the world, windy weather that shakes the buildings housing the interferometer instrumentation, microseismic vibrations

from ocean waves crashing on the shores of the Pacific Ocean, Atlantic Ocean, and the Gulf of Mexico, and local anthropogenic activity.^{6,7} The study of the effects of seismic activity was especially important for improving the data quality of transient gravitational wave searches in the initial LIGO era.^{8,9} One of the key improvements from initial to Advanced LIGO is the implementation of a much more sophisticated seismic isolation system, which includes stages of active and passive isolation for all of the cavity optics.^{2,10}

It is important to verify that this entirely new system provides the very high isolation expected and that it does not introduce any new types of transient noise that could add to the noise background for searches of short-duration gravitational waves, such as signals from black hole mergers and supernovae. Here we present an investigation of the transient motion of the Livingston suspension systems as measured by local sensors on each suspension, specifically looking at the displacement of the quadruple stage pendulums in the longitudinal degree of freedom, which is the direction of the optical path used to sense spacetime strain induced by passing gravitational waves.

II. ADVANCED LIGO SUSPENSIONS

In Advanced LIGO, all optical cavities use optics suspended from multi-stage pendulums, in order to benefit from

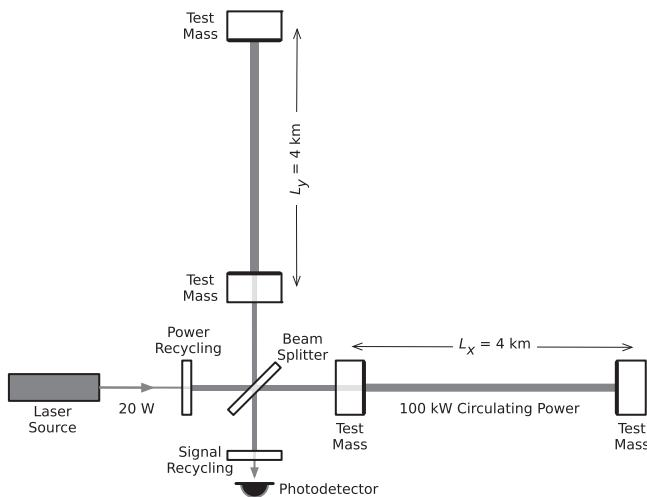


FIG. 1. Simplified diagram of the Advanced LIGO optical configuration, adapted from B. P. Abbott *et al.*, “Observation of gravitational waves from a binary black hole merger,” *Phys. Rev. Lett.* **116**, 061102 (2016). Copyright 2016 Author(s), licensed under a Creative Commons Attribution 3.0 Unported License.⁴ As a gravitational wave impinges upon the interferometer, it stretches and squeezes the arms of the interferometer, creating differential cavity length variations that are sensed by the photodetector. To reduce the effects of seismic motion on the measurement of strain, the mirrors at the input and end of both arms are suspended from quadruple-stage pendulums, in addition to active seismic isolation systems.

the lowpassing of seismic motion. The input and end mirrors (the optics whose motion most directly contributes to the gravitational-wave readout signal) are all hung from quadruple-stage suspensions,¹⁰ with each stage providing additional isolation at frequencies above the suspension resonances, which range from 0.4 Hz to 14 Hz. The quadruple pendulum is suspended at the top from maraging steel blade springs, with two further sets of springs incorporated into the top two masses, thus providing three stages of enhanced vertical isolation. The two lower masses of the quadruple

suspension are cylindrical silica masses connected by fused silica fibers to reduce thermal noise. Another similar quadruple suspension is hung next to the test mass suspension, so the actuation on lower stages can be done from a similarly isolated reaction chain. Figure 2 gives an overview of the design of the Advanced LIGO quadruple suspensions.

The local displacement of the top three stages of the suspensions is measured using Optical Sensor and Electro-Magnetic actuators, or OSEMs, which are electromagnetic sensors and actuators used for damping the suspensions’ resonances and controlling the mirrors to keep cavities aligned and locked.^{10,11} The lowest stage on each quadruple suspension does not have the OSEM sensors, but instead is controlled by an electrostatic drive.

The OSEMs can sense suspension motion at low frequencies where the displacements are relatively large. At frequencies above 5 Hz, the suspension motion has typically fallen below the sensitivity level of the OSEMs such that the resulting spectra are dominated by electronics noise. Multiple OSEMs on each stage allow the calculation of the mass’s motion in each degree of freedom using a linear combination of the sensors’ signals. The sensed displacement of the top stage is used in a feedback loop to actuate on that stage of the suspension in order to damp the mechanical resonances of the suspension. The sensors at lower stages are only used as witnesses of the optics’ displacement for the purposes of diagnosing problems in the suspensions. The actuators on lower stages use interferometer and cavity signals to keep various degrees of the interferometer precisely on resonance.

III. MOTION TRANSIENTS IN SUSPENSIONS

In order to eliminate false positives from the gravitational wave searches, it is necessary to understand the origins of non-astrophysical noise transients in the gravitational wave data. Each subsystem of the detector itself is therefore investigated in great detail to fully study all potential noise sources.⁷

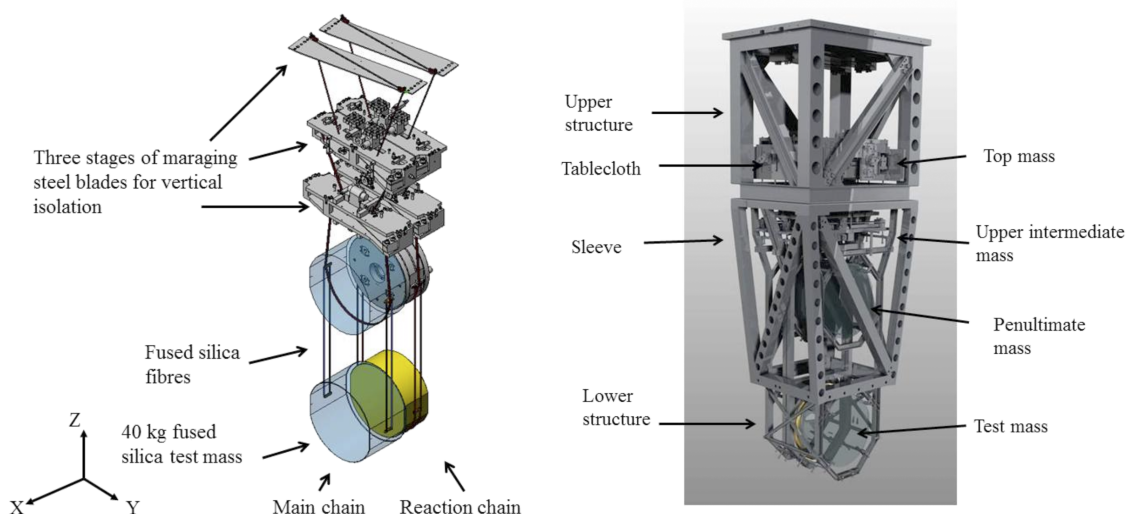


FIG. 2. Quadruple suspension design. Reprinted with permission from S. M. Aston *et al.*, “Update on quadruple suspension design for advanced LIGO,” *Classical Quantum Gravity* **29**, 235004 (2012). Copyright 2012 IOP Publishing.¹⁰ The left image shows the suspension systems with the blades, fibers, and reaction chain. On the right, the whole structure is shown, with the four masses labeled.

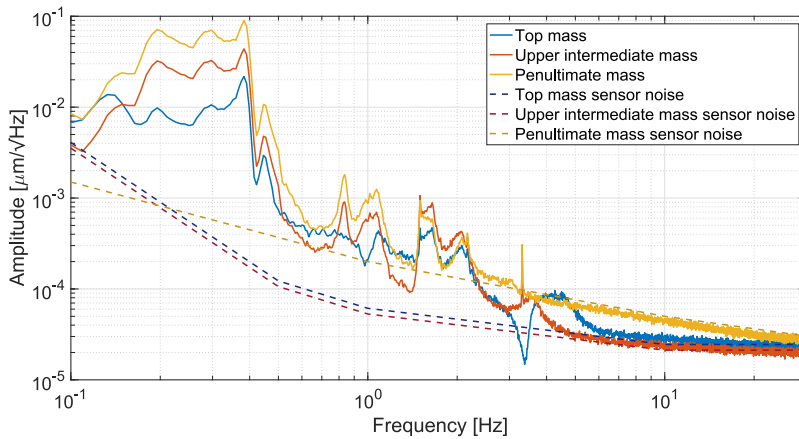


FIG. 3. Typical amplitude spectral density (ASD) for the Y-arm input test mass suspension (ITMY) longitudinal motion monitors during the first Advanced LIGO observing run. The spectra below the suspension resonances are dominated by seismic motion, and other low frequency features of the ASDs correspond to the pendulum resonances and the control loops used to damp them. Since this is during a time when suspension modes were damped and not excited, not every resonance of the system shows up in the ASD. For example, the pitch mode near 2.7 Hz is not visible here. The smooth portion of the ASD above 5 Hz shows where the electronics noise of the sensors dominates the spectrum. Since the penultimate stage requires a lower actuation force than the top mass, it uses a more lightweight type of actuator, which has slightly higher sensing noise floor at higher frequencies.¹¹

In this article, we characterize transients in the displacement of the suspensions' stages as measured by the OSEMs, the propagation of transients between different stages, and their effects on the gravitational wave strain data. Specifically, transients in the longitudinal degree of freedom were studied in the top three stages of the quadruple suspensions. The angular motion of the test masses is sensed using optical levers, but since these sensors do not measure the longitudinal motion, they are not used in this study.

Motion transients seen by the local displacement sensors have a few potential sources. For example, they could be caused by motion that is intrinsic to the suspension systems themselves, from the crackling in the suspension wires or the steel blades.^{12,13} Transients could also come from excess seismic motion by propagating through each stage of active seismic isolation and then down through the suspension stages. Above the suspension's resonance f_0 , the seismic transients should decrease in amplitude by a factor of $(f/f_0)^2$ at each stage and be less likely to appear above the sensor noise at

lower stages. Therefore any seismic transients that affect multiple stages should appear mostly at low frequencies. Another source of transients seen in the local sensors is the actuation on the suspensions from the feedback loops used to control the interferometer.

A. Suspension behavior in Advanced LIGO's first observing run

The typical spectrum of the suspension motion monitors is characterized by several peaks near the low frequency pendulum resonances between 0.4 and 5 Hz, and the smooth noise above 5 Hz due to the sensors' electronics noise. The main resonances in the longitudinal degree of freedom are modeled for the quadruple suspensions to be at 0.435 Hz, 0.997 Hz, 2.006 Hz, and 3.416 Hz, but coupling from other degrees of freedom and the active seismic isolation system creates additional peaks in the spectrum. Figure 3 shows a typical spectrum of the Y-arm input quadruple suspension (Input Test Mass Y or ITMY) motion in O1 along with estimated sensor noise levels.

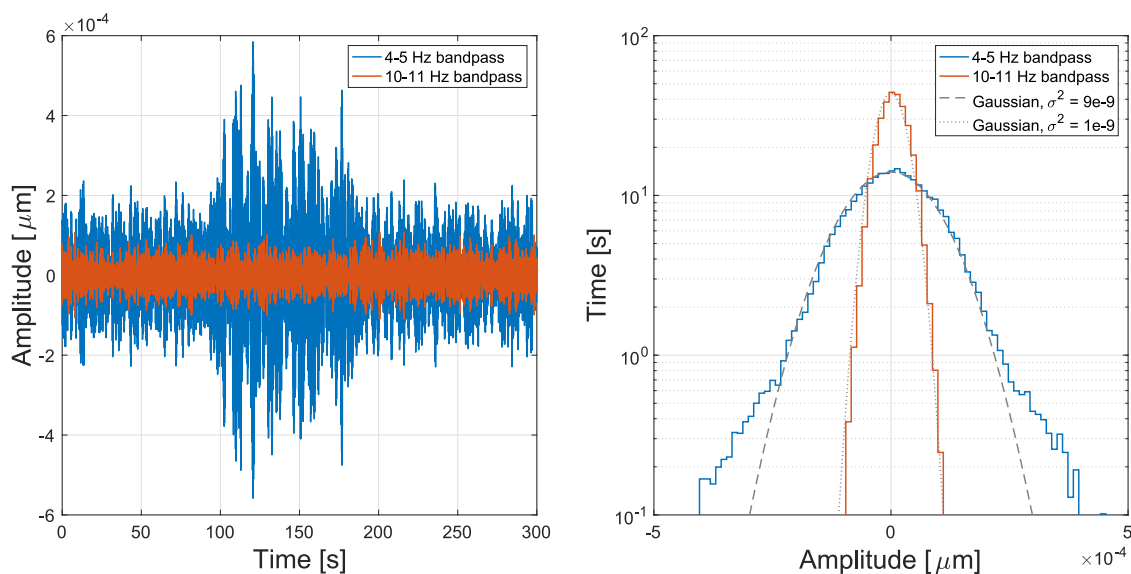


FIG. 4. The panel on the left shows a 5 min time series from the top stage of the ITMY suspension, with bandpass filters applied between 4 to 5 Hz and 10 to 11 Hz. The distribution of time series amplitude over the same time is shown on the right, with dashed lines to indicate a Gaussian distribution. While the Gaussian-distributed stationary sensor noise dominates the higher frequency band shown, the time series from 4 to 5 Hz exhibits large excursions from the average noise level.

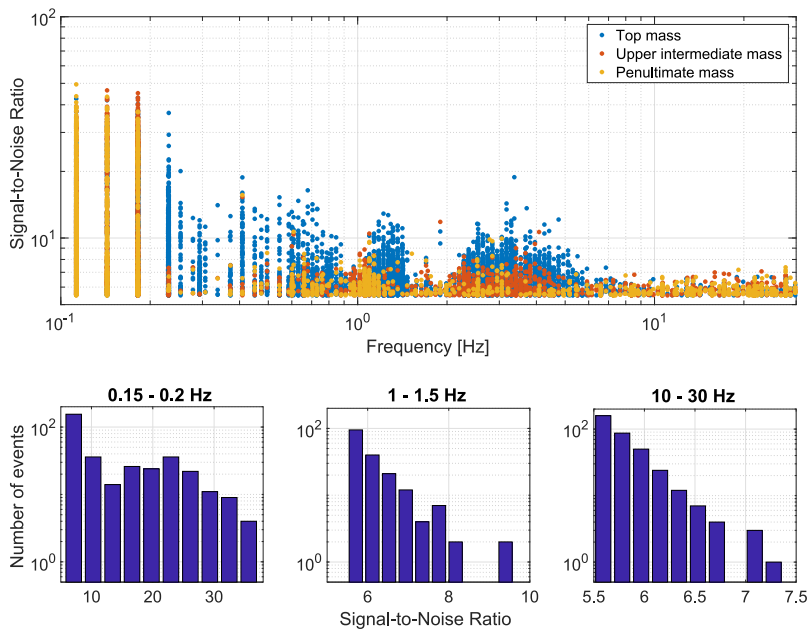


FIG. 5. (Top) The Signal-to-Noise Ratio (SNR) and central frequencies of Omicron triggers of the ITMY suspension during one week of O1. (Bottom) Histograms showing the SNR distributions of the penultimate stage triggers at three representative frequency ranges (note the different SNR scales), selected to show how transient behavior differs across the spectrum. While the distribution of higher frequency triggers fall off much like Gaussian noise, the lower frequency ranges contain more outliers.

Ideally, the noise would be stationary and the average spectrum would statistically characterize the noise level, but in actuality there are non-stationary disturbances at different frequencies. To demonstrate this, Fig. 4 shows the time series of several minutes of data from the top stage of one suspension with two different bandpass filters applied to select for 4-5 Hz and 10-11 Hz. Above 10 Hz, the sensor noise dominates the signal and the resulting time series is Gaussian distributed, but the lower frequency shows large non-Gaussian transients.

Rather than visually inspecting time series, the Omicron algorithm is used to find transients in the data, producing *triggers* that indicate the time, frequency, amplitude, and signal-to-noise ratio of the transient noise.^{14,15} Figure 5 shows the distribution in frequency and signal-to-noise ratio of Omicron triggers for the longitudinal degree of freedom, using data from the Y-arm input suspension over one week of the observing run. While stationary noise would produce a background of low SNR triggers across all frequencies, the actual data from the suspension monitors show a varying structure in different

frequency bands. This suggests the presence of non-stationary noise sources.

B. Motion transient propagation

To characterize the effects of short duration disturbances in the upper stages of the suspensions on the motion lower in the suspension chain, we need more than just the frequency domain models usually used to characterize the suspensions due to the influence of the impulse response of the system. The MATLAB Simulink toolbox¹⁶ was used to model the response of a simple pendulum to a sine-Gaussian input signal. Note that the input signal is not a pure sine wave at a single frequency, but rather a sine-Gaussian wave characterized by a peak frequency with a Gaussian amplitude envelope that acts to truncate the signal in time, giving it broader frequency content. Therefore, as the pendulum response more strongly attenuates the higher frequencies of the input signal, the peak frequency of the resulting motion is a mixture of the driving and the resonance frequencies, as demonstrated in Fig. 6.

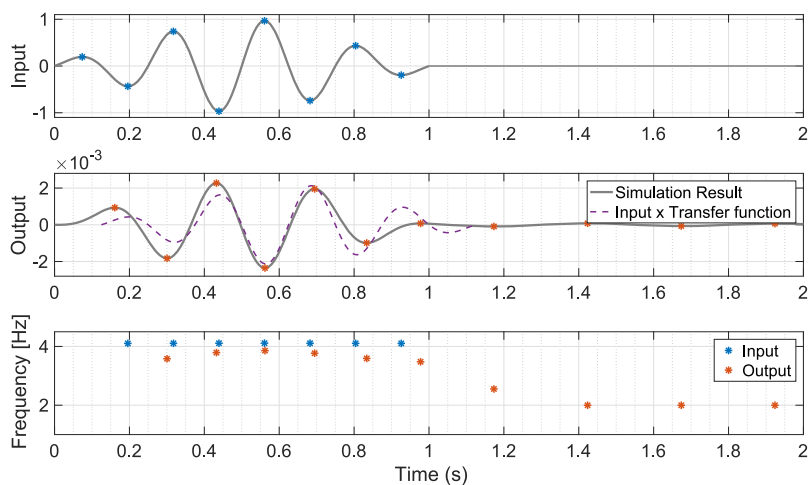


FIG. 6. Modeled transient response of a simple pendulum to a sine-Gaussian injection. Simulink was used to model a simple pendulum with a resonance at 2 Hz. A one-second 4 Hz sine-Gaussian signal (top panel) was used as the input to show the response of the system (middle panel) compared with the input signal multiplied by the transfer function of the system at 4 Hz. Local maxima and minima of the time series can be used to calculate the frequency for each half-cycle (bottom panel). This simulation shows that even for this simple model, the transient response of the system deviates from the steady state frequency response at 4 Hz.

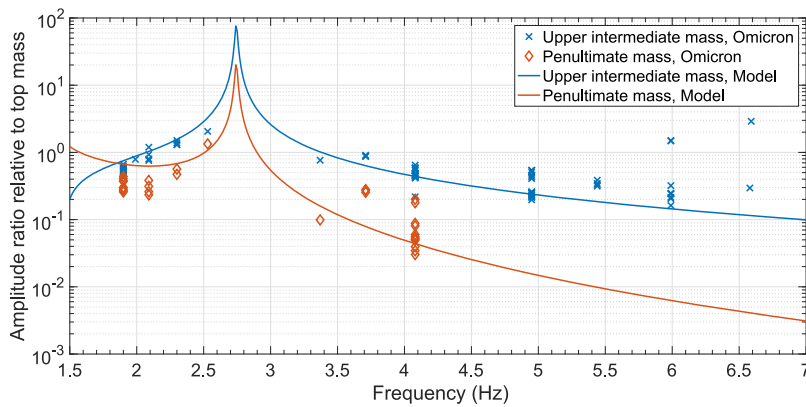


FIG. 7. Ratio of amplitudes of injection Omicron triggers at lower stages to the top stage, plotted against the peak frequency estimated by Omicron for the top stage motion, compared with the modeled transfer function. At lower frequencies, the propagation of the transients is close to the model, but above a few Hz, the motion at the lower stages is smaller than the sensor noise, and the amplitude ratio is not as close to the model. There are fewer Omicron triggers at the penultimate stage since the motion at that stage is at a lower amplitude and is not great enough at higher frequencies to be seen above the sensor noise.

To examine the propagation of transients in Advanced LIGO suspensions and compare with expected behavior, sine-Gaussian waveforms were physically injected in the Y-end quadruple suspension (End Test Mass Y or *ETMY*) in the longitudinal direction using the top mass actuators, with central frequencies ranging from 2 to 10 Hz. The Omicron algorithm was used to characterize the resulting transients caused in the top stage as well as in lower stages.

Figure 7 shows the ratio of the Omicron trigger amplitudes of the lower suspension stages to the top stage for different frequencies, using the Omicron frequency estimate of the top stage trigger. The solid lines show the frequency response of the suspensions as predicted by the quadruple suspension models. One reason for apparent discrepancies from the model is variation of the transient motion frequency between stages, as well as the fact that the motion at each stage is not characterized by only a single frequency. To analyze this effect, time series of the injections were examined individually to characterize the frequencies and amplitudes of the signals at each stage, similar to the process used in analysis of the Simulink model shown in Fig. 6.

Using a bandpass filter with a 1 Hz window around the injection frequency and finding the local maxima and minima of the resulting time series, the peak frequency of the induced transient motion was estimated with each cycle. Similar to the simulation performed in Simulink, the suspension's response is not exactly at the peak sine-Gaussian frequency, and when the injection is finished, the suspension's motion begins to ring

down with a frequency approaching the nearest resonance. As the motion propagates downwards, the pendulum filter response attenuates the signal more in the frequency range farther from the resonance, resulting in a slight frequency shift towards the resonance at the lower stage. Figure 8 shows the period increasing in the bandpassed time series from one of the injections. The 1 Hz bandpass filter was chosen to most clearly show the injected signal in the time series, but results are consistent with the use of other bandpass widths, such as 2 Hz.

The bandpass filter reduces the noise so that the time series cycles can be clearly determined. The frequency of the resulting motion at each stage was then estimated by taking the mean frequency, weighting each cycle by the amplitude of its maximum or minimum. The amplitude of motion was calculated using Omega, a multi-resolution technique for studying transients related to Omicron.^{14,15} Using the weighted average frequency and the amplitudes calculated by Omega, the ratio of motion transient amplitudes between suspension stages for each frequency can be better compared to the suspension model. Figure 9 displays this comparison for the propagation of the motion from the top stage to the second and third stages. Since the transient amplitude is much smaller at higher frequencies for each successive stage, the higher frequency injection measurements are farther from the model due to the sensor noise at the lower stages. In both lower stages, we see a shift in the frequency away from the frequency at the top stage, generally closer to the nearest suspension resonance, a pitch mode at 2.7 Hz.

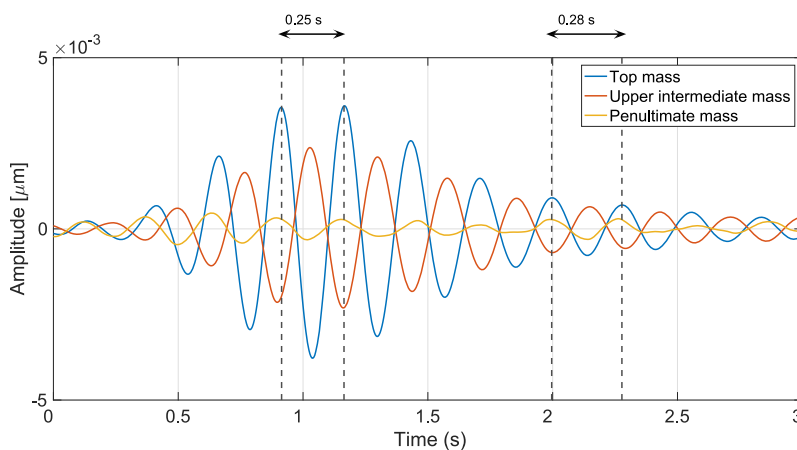


FIG. 8. Time series from one injection at 4.1 Hz, after application of a bandpass filter with a window of 1 Hz around the injection frequency. Similar to the simple pendulum model analysis, the frequency shifts throughout the time series. The period of the cycles in the top stage lengthens slightly, from 0.25 s (4.0 Hz) at the peak of the transient to 0.28 s (3.6 Hz) a few cycles later.

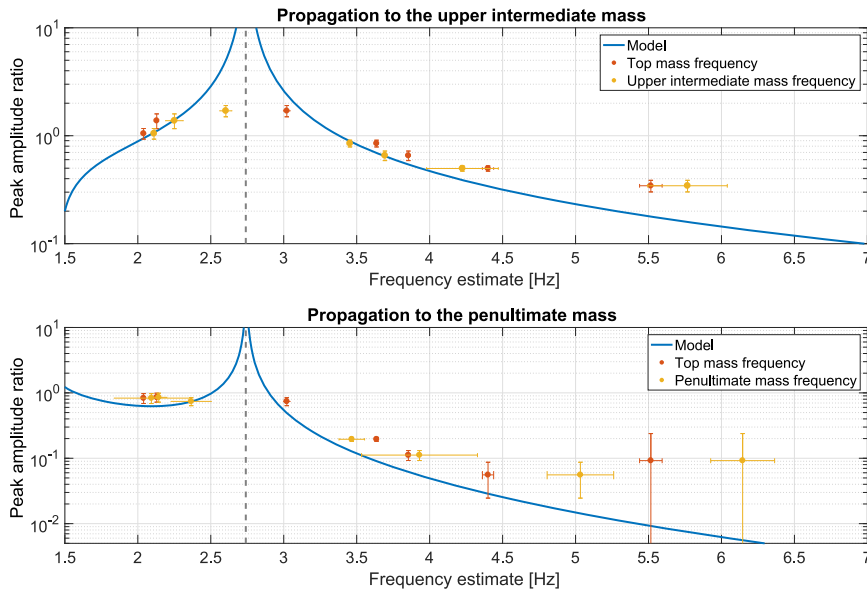


FIG. 9. Amplitude ratios as calculated by the Omega algorithm, and frequency estimated using the maxima and minima of bandpassed time series. Errors are greater as sensor noise becomes dominant at higher frequencies. Red and yellow points represent the same amplitude ratios between stages, but red points show the frequency estimate at the top stage while yellow points show the frequency estimate at the lower stages. Error bars shown are the standard deviation of the measurement among the various injections of the same frequency, weighted by the amplitude of the injection at the top stage.

Having explored the propagation of short transients in the suspension stages, we turn now to studying the effect of the actual suspension transients on the LIGO gravitational wave strain data during the first Advanced LIGO observing run.

C. Correlations with gravitational wave strain data

Taking the data from the first week of November (the same week shown in Fig. 5), Omicron was used to identify transients in the gravitational wave (GW) strain data in the same frequency range as used to produce the suspension motion triggers (0.1–60 Hz), as well as at higher frequencies to check for any nonlinear coupling. Figure 10 shows the Receiver Operator Characteristics (ROC) curves,¹⁷ showing the fraction of GW triggers with times within a given time window (ranging

from 0.1 to 10 s) of triggers in the ITMY longitudinal displacement data. This fraction is compared with the fraction of time coincidences that would occur by chance between uncorrelated data sets (false alarm). The rate of random coincidences is estimated by performing twenty one-second time shifts between the two data sets (10 s in either direction) and finding the fraction of triggers with a time difference within the given time window. The fraction of coincident triggers in each time-shifted set of data are averaged together to give the false alarm. In both frequency ranges, the small number of coincidences between the sets of data is consistent with the number that would be expected by random chance. The observed transients in the ITMY suspension motion monitors did not show any significant correlation with GW strain noise transients, at any frequency.

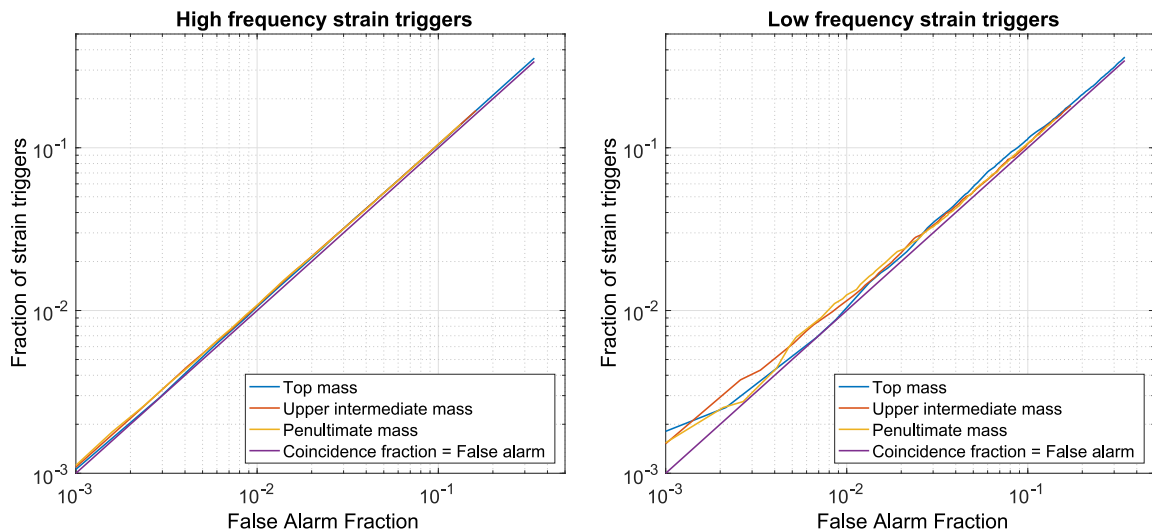


FIG. 10. Receiver Operator Characteristic (ROC) curves showing the correlation between noise transients in the GW strain and ITMY suspension data from November 1 to 8, 2015. The left-hand plot shows the correlation with higher frequency GW strain triggers (above 60 Hz), while the plot on the right shows the correlation with GW strain triggers below 60 Hz. The y axis shows the fraction of triggers coincident between the two sets of data for varying time windows. The x axis represents the number of coincidences that would appear by chance, estimated by repeating the analysis at each time window with different time shifts between the two data sets. For both sets of GW strain triggers, the coincidence rate is approximately equal to the false alarm rate, as would be expected for uncorrelated random events, whereas a significant correlation would have a much greater efficiency than the false alarm rate.

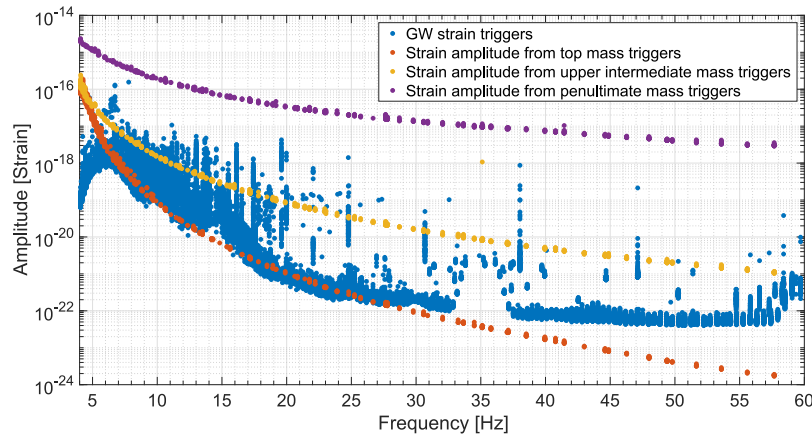


FIG. 11. Livingston ITMY Omicron triggers from a week in the first observing run, multiplied by the transfer function to the lowest stage and divided by the arm length to convert the displacement into equivalent strain amplitude. The strain calibration of the gravitational wave data is only accurate above 10 Hz, at frequencies where the OSEM signals are dominated by sensor noise. Therefore, this calculation can only give us the upper limit of transient motion from each stage that could appear in the GW strain data without also appearing in the local displacement sensor. Where there are GW strain noise transients above one of these levels, we can rule out an origin in a particular stage of the suspension chain. A large number of the GW strain triggers are above the noise level from the top stage (84% of the triggers between 10 and 60 Hz), eliminating the origin of these transients at the top of the suspension chain. However, only the very loudest GW strain triggers are above the level of the second stage (3.2% of the triggers between 10 and 60 Hz), and no GW strain triggers are higher than the level of the third stage.

Although the observed transients in the suspension monitors are not correlated with GW strain transients, it is possible that there are additional suspension noise transients with amplitude below the sensor noise. Upper limits can be set on the possible effect of such suspension transients on the GW strain. The amplitude of the Omicron triggers from each of the upper stages of ITMY is multiplied by the suspension transfer function to estimate the amplitude of noise transients that would be caused in the test mass by a physical displacement of that amplitude. Figure 11 shows the resulting projections in the equivalent GW strain amplitude, alongside the GW strain triggers from the same time. The sensor noise at the lower stages is much higher than the expected amplitude of motion at those stages, so the upper limit of motion at the lowest stage is above most of the GW strain triggers. The noise level predicted by the top stage triggers, however, is below most of the GW strain triggers, so if noise originating in that stage caused high amplitude transients in the GW data, it would be expected to also be seen by the top stage sensors.

Since the top stage triggers are not statistically correlated with any of the GW strain triggers, we can conclude that transient noise originating at the top stage of the suspension is not a significant contribution to the transient noise in the interferometer. We cannot, however, rule out the possibility of GW strain noise transients caused by motion originating in the lower stages of the suspension, since there are a significant portion of GW strain triggers that fall below the level of transient noise caused by the local sensor noise.

IV. CONCLUSIONS

Using short duration hardware injections in the top stage of the suspension, we have studied the propagation of transient motion down the suspension chain. The difference of transient amplitudes at different stages is consistent with the

models, although slight variations in frequency must be taken into account. The frequency of the transients shifts because the injected waveform is not a pure sine wave but a sine-Gaussian, and after the short duration injection, the suspension motion oscillates with a decreasing amplitude and frequency that shifts toward the closest mechanical resonance frequency. Transients at different stages of the suspension therefore show slightly different frequencies from the same initial sine-Gaussian injection.

Statistical comparisons of the times of transients in the OSEMs and in the GW strain data during O1 show that transients seen by the local displacement sensors of the suspensions are not a significant source of background transient noise in the interferometer. However, this does not rule out transient suspension motion that is below the local sensor noise as a possible source of background noise. Using the suspension models to propagate the sensor noise into the motion at the test mass, upper limits can be placed on the level of noise that could be caused in the GW strain data from transients in suspension motion at each stage. Most GW strain triggers are above the sensor noise level of the top stage of the suspension, but below the noise level of the second and third stages. Here transient propagation from upper stages to lower has been explored. Possible sources of noise in the lower stages of the suspensions that are currently being studied include crackle noise in the suspension fiber^{12,13} and Barkhausen noise.^{9,18} Transient noise that originates in the lower stages of the suspension could therefore be a cause of noise in the GW data while not being loud enough to appear above the local sensor noise.

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